

1. Dispersion and Abbe number

- a. What kind of Abbe V number offers large dispersion

Ans: A small Abbe V number has a large dispersion

- b. What is the sign of the Abbe V number for a glass with:

- i. Negative dispersion
- ii. Positive dispersion
- iii. No dispersion

Ans: Since the formula for Abbe V number is:

$$V = \frac{n_d - 1}{n_F - n_C}$$

Where n_d is always greater than 1, so the numerator is always positive. So the sign of the Abbe number depends on the denominator. The denominator is positive when n_F is greater than n_C and is negative when the reverse is true.

In addition, n_F is at 486.1nm and n_C is at 656.3nm. thus:

- i. Negative dispersion: n_F is smaller than n_C , so Abbe number is negative
- ii. Positive dispersion: n_F is larger than n_C , so Abbe number is positive
- iii. No Dispersion, the Abbe number becomes infinite (could be negative or positive)

- c. Find 3 glasses from a catalogue (mention the source) with

- i. Negative dispersion
- ii. Positive dispersion
- iii. Minimum dispersion

Ans: Answers are based on Schott's Abbe diagram:

[http://www.us.schott.com/advanced_optics/english/download/schott_abbe_n_d_vd_pgf_july_2011_us.pdf?highlighted_text=abbe diagram](http://www.us.schott.com/advanced_optics/english/download/schott_abbe_n_d_vd_pgf_july_2011_us.pdf?highlighted_text=abbe%20diagram)

- i. Negative dispersion does not exist on the chart

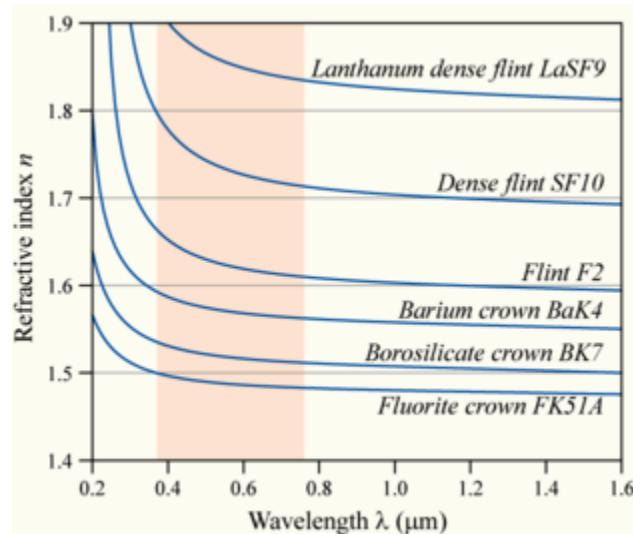
From Wikipedia: [http://en.wikipedia.org/wiki/Dispersion_\(optics\)](http://en.wikipedia.org/wiki/Dispersion_(optics))

Negative dispersion is usually achieved by prism-pairs, diffraction gratings, or chirped mirrors with coatings design at certain wavelength(s)

- ii. Positive dispersion: all material in the chart has positive dispersion
I chose P-SF68 for further study
(source: Schott
[http://www.us.schott.com/advanced_optics/english/download/schott_abbe_nd_vd_pgf_july_2011_us.pdf?highlighted_text=abbe diagram](http://www.us.schott.com/advanced_optics/english/download/schott_abbe_nd_vd_pgf_july_2011_us.pdf?highlighted_text=abbe%20diagram))
- iii. Minimum dispersion: the smallest dispersion, which has the highest Abbe number is N-FK51A (V is about 85)
(source: Schott
[http://www.us.schott.com/advanced_optics/english/download/schott_abbe_nd_vd_pgf_july_2011_us.pdf?highlighted_text=abbe diagram](http://www.us.schott.com/advanced_optics/english/download/schott_abbe_nd_vd_pgf_july_2011_us.pdf?highlighted_text=abbe%20diagram))

d. What can we say about dispersion of a glass in IR range based on its Abbe V number?

Ans: Since the Abbe number is only useful for wavelength from 486.1nm to 656.3nm and IR is from 10^{-3} to 10^{-6} m or 10^6 to 10^3 nm, the behavior must be extrapolated. From Wikipedia ([http://en.wikipedia.org/wiki/Dispersion \(optics\)](http://en.wikipedia.org/wiki/Dispersion_(optics))) the relationship of Refractive index to wavelength for most glass material tends to flatten out at longer wavelength:



One could predict that the dispersion at IR range will be smaller

e. Find the catalogue information for a low and high dispersion glass and explain meaning of the information listed for them.

Ans: from Schott:

N-SF68 (a material with low V number) is at:

http://www.us.schott.com/advanced_optics/english/our_products/materials/d_ata_tools/index.html

Key Information presented are:

Refractive indices at selected wavelengths

Internal transmittance at selected wavelengths for 10mm and 25mm

Relative Partial Dispersion: this is similar to the Abbe number but defined at different wavelength

SCHOTT			OPTICAL GLASS			SF	
P-SF68 005210.619			$n_d = 2.00520$ $n_e = 2.01643$	$\nu_d = 21.00$ $\nu_e = 20.82$	$n_F - n_C = 0.047867$ $n_F' - n_C' = 0.048826$		
Refractive Indices			Internal Transmittance τ_i			Relative Partial Dispersion	
	λ [nm]		λ [nm]	τ_i (10mm)	τ_i (25mm)		
$n_{2325,4}$	2325,4	1.93381	2500	0.793	0.560	$P_{s,t}$	0.1885
$n_{1970,1}$	1970,1	1.93968	2325	0.905	0.780	$P_{c,s}$	0.4406
$n_{1529,6}$	1529,6	1.94732	1970	0.976	0.940	$P_{d,c}$	0.2817
$n_{1060,0}$	1060,0	1.95970	1530	0.996	0.990	$P_{e,d}$	0.2346
n_t	1014,0	1.96160	1060	0.999	0.998	$P_{g,F}$	0.6392
n_s	852,1	1.97063	700	0.997	0.993	$P_{t,h}$	
n_r	706,5	1.98449	660	0.996	0.989		
n_c	656,3	1.99171	620	0.994	0.985	$P'_{s,t}$	0.1848
n_c'	643,8	1.99380	580	0.989	0.973	$P'_{c,s}$	0.4746
$n_{632,8}$	632,8	1.99576	546	0.976	0.940	$P'_{d,c'}$	0.2336
n_D	589,3	2.00479	500	0.905	0.780	$P'_{e,d'}$	0.2300
n_d	587,6	2.00520	460	0.758	0.500	$P'_{g,F'}$	0.5644
n_e	546,1	2.01643	436	0.574	0.250	$P'_{t,h}$	
n_F	486,1	2.03958	420	0.302	0.050		
n_F'	480,0	2.04262	405	0.036		Deviations of Relative Partial Dispersion ΔP from the "Normal Line"	
n_g	435,8	2.07018	400	0.007		$\Delta P_{c,t}$	-0.0156
n_h	404,7		390			$\Delta P_{c,s}$	-0.0113
n_i	365,0		380			$\Delta P_{F,e}$	0.0063
$n_{334,1}$	334,1		370			$\Delta P_{g,F}$	0.0308
$n_{312,6}$	312,6		365			$\Delta P_{t,g}$	
$n_{296,7}$	296,7		350			Other Properties	
$n_{280,4}$	280,4		334			$\alpha_{30/+70^\circ C} [10^{-6}/K]$	8.4
$n_{248,3}$	248,3		320			$\alpha_{+20/+300^\circ C} [10^{-6}/K]$	9.7
			310			T_g [$^\circ C$]	428
Constants of Dispersion Formula			300			$T_{10^{13,0}}$ [$^\circ C$]	430
B_1	2.3330067		290			$T_{10^{7,6}}$ [$^\circ C$]	504
B_2	0.452961396		280			c_p [(g·K)]	0.370
B_3	1.25172339		270			λ [W/(m·K)]	0.650
C_1	0.0168838419		260			ΔT [$^\circ C$]	468
C_2	0.0716086325		250			ρ [g/cm ³]	6.19
C_3	118.707479					E [10 ³ N/mm ²]	79
Constants of Formula for dn/dT			Color Code				
D_0	$1.55 \cdot 10^{-5}$		λ_{80}/λ_5	49/41*			
D_1	$2.30 \cdot 10^{-8}$		Remarks				
D_2	$-3.46 \cdot 10^{-11}$		suitable for precision molding				
E_0	$2.76 \cdot 10^{-8}$						
E_1	$2.93 \cdot 10^{-9}$						
λ_{TK} [μm]	0.297						
Temperature Coefficients of Refractive Index							
	$\Delta n_{rel}/\Delta T$ [10 ⁻⁶ /K]			$\Delta n_{abs}/\Delta T$ [10 ⁻⁶ /K]			
[$^\circ C$]	1060,0	e	g	1060,0	e	g	
-40/-20	13.7	21.5	32.3	11.1	18.8	29.5	AR
+20/+40	15.2	24.1	36.5	13.5	22.3	34.6	PR

Similar information can be found for N-FK51A

SCHOTT			OPTICAL GLASS			FK	
N-FK51A 487845.368			$n_d = 1.48656$ $n_e = 1.48794$	$\nu_d = 84.47$ $\nu_e = 84.07$	$n_F - n_C = 0.005760$ $n_F' - n_C' = 0.005804$		
Refractive Indices			Internal Transmittance τ_i			Relative Partial Dispersion	
	λ [nm]		λ [nm]	τ_i (10mm)	τ_i (25mm)		
n _{2325,4}	2325,4	1.46958	2500	0.891	0.750	P _{s,t}	0.2879
n _{1970,1}	1970,1	1.47271	2325	0.933	0.840	P _{c,s}	0.5465
n _{1529,6}	1529,6	1.47608	1970	0.976	0.940	P _{d,c}	0.3062
n _{1060,0}	1060,0	1.47959	1530	0.992	0.980	P _{e,d}	0.2388
n _t	1014,0	1.47999	1060	0.998	0.994	P _{g,f}	0.5359
n _s	852,1	1.48165	700	0.998	0.995	P _h	0.7429
n _r	706,5	1.48379	660	0.998	0.995		
n _c	656,3	1.48480	620	0.998	0.996	P' _{s,t}	0.2858
n _{c'}	643,8	1.48508	580	0.999	0.997	P' _{c,s}	0.5909
n _{632,8}	632,8	1.48534	546	0.999	0.997	P' _{d,c'}	0.2554
n _D	589,3	1.48651	500	0.998	0.996	P' _{e,d}	0.2370
n _d	587,6	1.48656	460	0.997	0.993	P' _{g,f'}	0.4759
n _e	546,1	1.48794	436	0.997	0.992	P' _h	0.7373
n _F	486,1	1.49056	420	0.997	0.992		
n _{F'}	480,0	1.49088	405	0.997	0.993		
n _g	435,8	1.49364	400	0.997	0.993	Deviation of Relative Partial Dispersion ΔP from the "Normal Line"	
n _h	404,7	1.49618	390	0.997	0.992	$\Delta P_{c,t}$	-0.1112
n _i	365,0	1.50046	380	0.995	0.988	$\Delta P_{c,s}$	-0.0533
n _{334,1}	334,1	1.50501	370	0.990	0.976	$\Delta P_{F,e}$	0.0110
n _{312,6}	312,6	1.50911	365	0.985	0.963	$\Delta P_{g,f}$	0.0342
n _{296,7}	296,7		350	0.948	0.875	$\Delta P'_{i,g}$	0.1675
n _{280,4}	280,4		334	0.831	0.630		
n _{248,3}	248,3		320	0.618	0.300		
			310	0.428	0.120		
Constants of Dispersion Formula			300	0.262	0.035	Other Properties	
B ₁	0.971247817		290	0.137	0.010	$\alpha_{-30/+70^\circ C}$ [$10^{-6}/K$]	12.7
B ₂	0.216901417		280	0.058		$\alpha_{+20/+300^\circ C}$ [$10^{-6}/K$]	14.8
B ₃	0.904651666		270			T _g [°C]	464
C ₁	0.00472301995		260			T ₁₀ ^{3,0} [°C]	463
C ₂	0.0153575612		250			T ₁₀ ^{7,5} [°C]	527
C ₃	168.68133					c _p [J/(gK)]	0.690
						λ [W/(mK)]	0.760
						AT [°C]	503
						ρ [g/cm ³]	3.68
						E [10 ³ N/mm ²]	73
						μ	0.302
						K [10 ⁻⁶ mm ² /N]	0.70
Constants of Formula for dn/dT			Color Code				
D ₀	-1.83 · 10 ⁻⁵		λ_{50}/λ_S	34/28			
D ₁	-7.89 · 10 ⁻⁹						
D ₂	-1.63 · 10 ⁻¹²						
E ₀	3.74 · 10 ⁻⁷		Remarks			K [10 ⁻⁶ mm ² /N]	
E ₁	3.46 · 10 ⁻¹⁰		suitable for precision molding			HK _{0,1/20}	
λ_{TK} [μm]	0.15					HG	
					HG-]		528
					B		1
					CR		1
					FR		0
					SR		52.3
					SR-]		2
Temperature Coefficients of Refractive Index							
	$\Delta n_{\text{rel}}/\Delta T$ [10 ⁻⁶ /K]		$\Delta n_{\text{abs}}/\Delta T$ [10 ⁻⁶ /K]				
[°C]	1060,0		1060,0				

2. Rule of thumb

Name for Rule	Speed of Light
The rule of Thumb	$c = 3 \cdot 10^8 \text{ m/s}$
When is this used	Most equations involving speed of light
Limitations	c is really 299,792,458 m/s; this rule of thumb gives 0.06% error, which is reasonable for most calculations; this should be avoided if more than 4-decimal precision is needed
Name for Rule	Thin lens analysis (a)
The rule of Thumb	wavefronts arriving at a thin lens are curved and stay in phase
When is this used	Ray tracing
Limitations	At different distances from the optical axis, the ray will travel through different amount of lens, thus exiting the lens with a slightly different shift in phase
Name for Rule	Thin lens analysis (b)
The rule of Thumb	the bending of the ray through a lens occurs at a single point
When is this used	Ray tracing
Limitations	This will not count the bending of the ray within a lens. This is sufficient with the width of the lens is much smaller than the object and image distance (about 10 times smaller)
Name for Rule	Fraunhofer Diffraction
The rule of Thumb	when a source or the observer is very far, the outgoing rays can be considered parallel
When is this used	Ray tracing
Limitations	This cannot be used when the object or image is question is relatively close to the lens (about 10 times the focal length)
Name for Rule	Small Angle Approximation (other version)
The rule of Thumb	$\cos \theta = 1$ (in radians)
When is this used	For small angles (< 0.2 radians) Application of this approximation greatly simplifies analysis and calculation
Limitations	$\cos(0.2) = 0.98$ which gives 2% error. The error will drastically increase as the angle increases

3. A camera focused between 1 meter and infinity

A point and shoot camera company claims their digital camera can take sharp images of the objects located between 1m and infinity. The pixel size is 3x3 (micron squared), lens aperture is 5mm in diameter, lens focal length is 10mm.

- a. Evaluate validity of the claim numerically for the green light (550nm). Draw diagrams if necessary.

Ans: first we calculate the diffraction limit of the system:

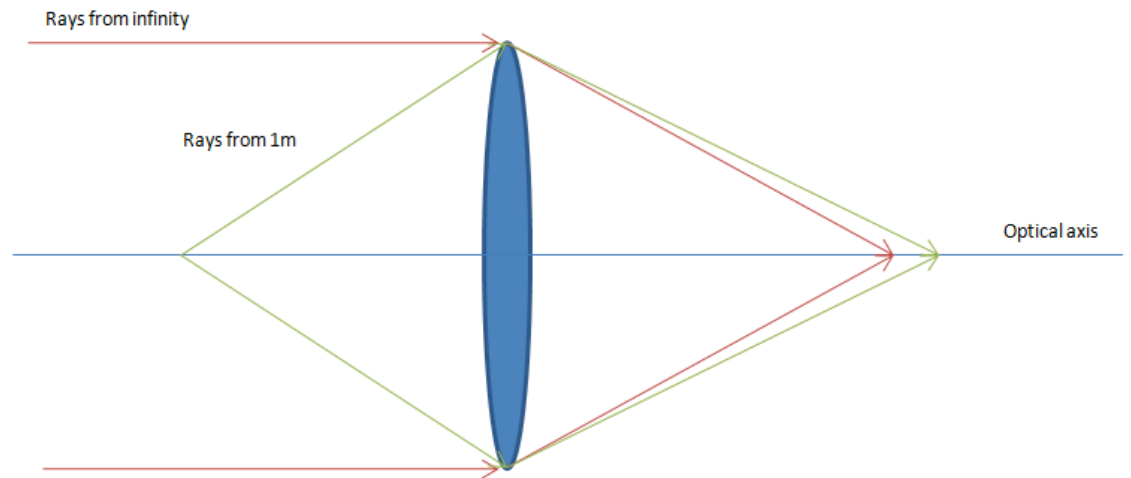
$$\Delta l = 1.220 \frac{f\lambda}{D}$$

so in this case the diffraction limit is $1.220 * 10 * 550\text{nm} / 5 = 1342\text{nm}$ or 1.342 micron (this is the best focus the system can have for green light)

Assuming the primary subject of the photograph is at 1m so the correct image distance is given by:

$$\frac{1}{S_1} + \frac{1}{S_2} = \frac{1}{f}$$

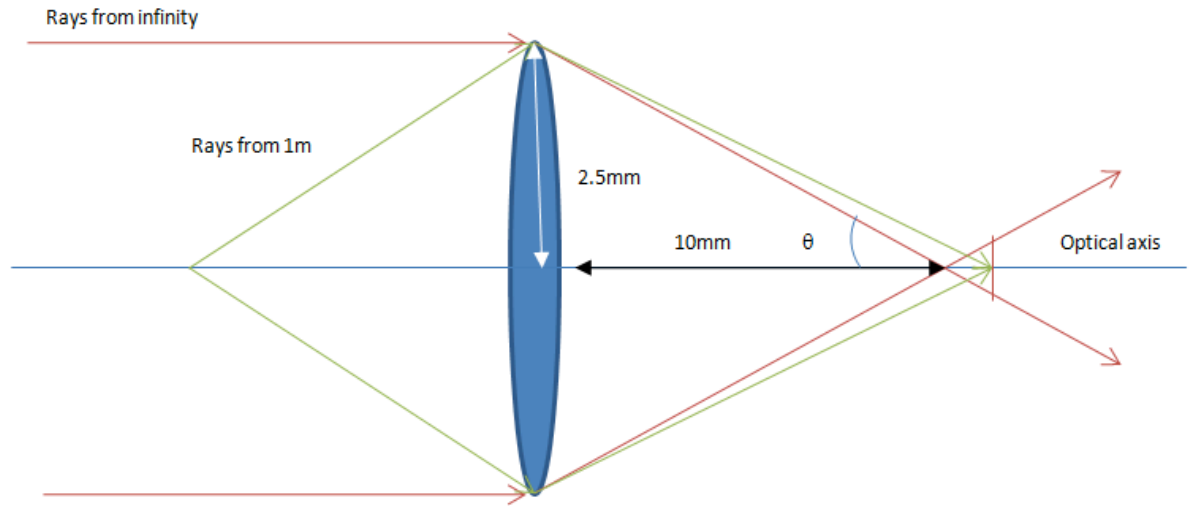
where $S_1 = 1\text{m}$ and $f = 10\text{mm}$ so S_2 is 10.1 mm and the object from infinity is of course focused at 10mm. So the difference between the two is 0.1 mm.



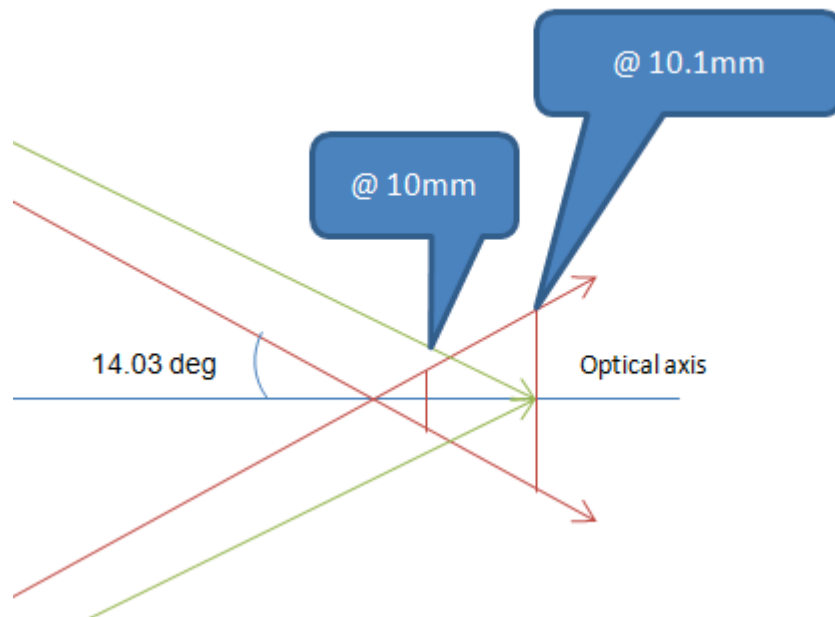
The question becomes what happens to the image from infinity at 10.1mm instead of 10mm. Using small angle the spot size becomes:

the angle between the optical axis and the ray is θ so that:

$$\tan \theta = 2.5/10 \quad \theta = 14.03 \text{ degrees}$$



so at 10.1mm the resolution becomes $1.342 + \tan(14.03) * 100 = 26.33$ microns, which is still much larger than 3 microns, so it cannot be in focus!



So trying some reverse calculation (since the aperture on a camera can be adjusted):

$$D = 1.22 * (10\text{mm}) * (0.55\mu\text{m}) / (3\mu\text{m})$$

$$D = 2.2367 \text{ mm}$$

$$\text{Theta} = 6.38 \text{ deg}$$

So the answers become (still not in focus):

D = 2.2367mm f = 10mm	wave length [nm]	resolution limit [nm]	@ 10.1 mm defocus [um] theta = 6.38 deg
blue light	450	2454.51	13.64
green light	550	2999.96	14.18
red light	750	4090.85	15.27

Ok, trying again with the primary object at 3 meters:

the following equation will yield:

$$\frac{1}{S_1} + \frac{1}{S_2} = \frac{1}{f}$$

S1 = 3000mm and f = 10mm so S2 = 10.033mm

and the table becomes:

D = 5mm f = 10mm	wave length [nm]	resolution limit [nm]	@ 10.033 mm defocus [um] theta = 14.03 deg
blue light	450	1098.00	9.34
green light	550	1342.00	9.59
red light	750	1830.00	10.08

These results still proves that the object from infinity is not in focus!

They are much closer.

There is the table again with the aperture closed down to allow green light to resolve at

3um:

D = 2.2367mm f = 10mm	wave length [nm]	resolution limit [nm]	@ 10.033 mm defocus [um] theta = 6.38 deg
blue light	450	2454.51	6.14
green light	550	2999.96	6.69
red light	750	4090.85	7.78

This is the smallest resolution I can get for objects at infinity and they are still not in focus.

- b. What happens when you consider red (750nm) and blue (450nm) light? For which wavelength the focus is better.

Ans: following the equations above:

the 750nm light has a diffraction limit of 1.830 microns and thus the de-focus of 10.1mm will be 26.82 microns

The 450nm light has a diffraction limit of 1.098 microns and at the de-focus of 10.1mm the size of resolution is 26.086 microns

Thus the blue light is easier to focus but is still not in focus

c. What if the diameter of the lens is 2.5mm and f is 5mm

Ans: everything is the same because the ratio between the diameter and the focus length is the same

d. What if the diameter of the lens is 10mm and the focal length is 10mm

Ans:

D = f = 10 mm	wave length [nm]	resolution limit [nm]	@ 10.1 mm defocus [um] theta = 26.56 deg
blue light	450	549	50.54
green light	550	671	50.66
red light	750	915	50.90

e. Organize your findings as a function of f# (f/D) and wavelength in the form of an easy rule to remember

Ans: as f# increases, image at infinity becomes clear (more in focus)
as wavelength decreases the image becomes more in focus
but the impact is much smaller than f#

I have recently purchased a SLR camera and this finding is consistent with introduction to photography. This also explains the lenses designed for portrait have very small f#.